## PERFORMANCE

## PERFORMANCE



Quick
Referrence
$H_{\text {andbook }}$

## PERFORMANCE

## WARNING

THE PERFORMANCE DATA IS BASED ON AN
AIRCRAFT THATIS:
1.) WELL MAINTAINED
2.) OPERATING NORMALLY
3.) EXPERTLY FLOWN

THERE ARE NO ALLOWANCES FOR POOR AIRCRAFT PERFORMANCE OR IMPROPER PILOT TECHNIQUE.

Copyright © 2010 by L29 Support, Inc.
INTRODUCTION
PURPOSE ..... 5.4
ORGANIZATION ..... 5.4
DATA SOURCE ..... 5.4
CORRECTIONS AND REVISIONS ..... 5.4
PAGE NUMBERS ..... 5.5
HANDBOOK RIGHTS ..... 5.5
DISCLAIMER ..... 5.5
CONTACT INFORMATION ..... 5.5
EXPLANATIONS
EXAMPLE ..... 5.6
FUEL QUANTITY AND WEIGHT ..... 5.7
TAXI FUEL ..... 5.8
STALL SPEEDS ..... 5.8
WIND COMPONENT CHART ..... 5.8
DENSITY ALTITUDE TABLE. ..... 5.9
TAKEOFF PERFORMANCE ..... 5.10
CLIMB PERFORMANCE ..... 5.12
CRUISE PERFORMANCE ..... 5.14
DESCENT PERFORMANCE ..... 5.15
APPROACH/HOLDING FUEL ..... 5.16
LANDING PERFORMANCE ..... 5.17
TABLES
FUEL QUANTITY AND WEIGHT. ..... 5.19
STALL SPEEDS ..... 5.20
WIND COMPONENT CHART ..... 5.21
DENSITY ALTITUDE TABLE ..... 5.22
TAKEOFF PERFORMANCE ..... 5.24
CLIMB PERFORMANCE ..... 5.26
CRUISE PERFORMANCE ..... 5.28
DESCENT PERFORMANCE ..... 5.31
LANDING PERFORMANCE ..... 5.32

## INTRODUCTION

## PURPOSE

To enhance safety by providing an L-29 pilot with an operational tool that facilitates acquiring performance data quickly in a user friendly format.

The performance data may be used for flight planning, determining fuel requirements specified in 14 CFR §§ 91.103(a), 91.151 or 91.167 and takeoff and landing performance information required by 14 CFR §91.103(b)(2).

## ORGANIZATION

The performance data was converted from graph form to a table format for simplification and functionality. The tables are laid out in the order a normal flight would progress.

## DATA SOURCE

The Nigerian Air force L-29 Flight Manual and the manufacturer's published data was the source for the performance data. No flight testing was performed to validate any of the performance data.

## CORRECTIONS AND REVISIONS

Considerable effort was put into this handbook to ensure accuracy. However, as with many things, errors may occur. Please help make this and future handbooks as error free as possible by reporting suspected errors to:

## corrections@L29support.com

The effective date and revision number are located on the footer of each page. When a revision is necessary the handbook will be revised in its entirety. Please consult the L29support.com web site to determine the current revision date and number.

## PERFORMANCE

The user of this handbook shall ensure that only the current version is used and, since this is not a controlled document, assumes all responsibility for the accuracy of the content contained herein.

## PAGE NUMBERS

The first number reflects the section number which corresponds to "Performance", in accordance with GAMA Specification No. 1, and the second number is the page number.

## HANDBOOK RIGHTS

This handbook is copyrighted material and may not be reproduced, copied, in whole or in part, without the express written consent of Thomas W. Lindee.

## DISCLAIMER

No warranty or guarantee, expressed or implied, is made as to the accuracy, sufficiency or suitability of the materials contained herein or any revision, supplement or bulletin hereto. It is understood and agreed to by the user of this handbook that they shall release indemnity and hold L29 Support, Inc. harmless against any and all claims or actions of whatever nature which may arise or claim to arise from the use hereof.

## CONTACT INFORMATION

If you have a comment, question or would like to acquire additional copies of this handbook please visit the web site L29support.com.

## EXPLANATIONS

Performance data may be obtained quickly and in doing so will, in most cases, offer additional pad for operational safety. The explanations for using the quick method will be in bold print following the word QUICK.

Performance data may also be obtained by the interpolation method. This method is somewhat arduous but will yield performance data which will accurately reflect the capabilities of the aircraft for the current conditions and is typically used when the quick method does not provide sufficient performance or exact data is desired.

## EXAMPLE

To help explain the use of the performance tables an example of a typical cross country flight is summarized and then explained in the following pages. Both the quick and interpolation methods are explained.

## EXAMPLE CONDITIONS:

| Pilots: 2 Distance: 275NM | Fuel: 1300L |
| :---: | :---: |
| DEPARTURE FIELD: |  |
| Elevation: 900'MSL | Altimeter setting: 29.82" |
| Temperature: $27^{\circ} \mathrm{C}$ | Wind: 360 @ 10kts. |
| Runway: 30L | Slope: 1\% Downhill |
| CRUISE: |  |
| 16,500' MSL | Wind: Calm |
| Temp: Missing (if unknown use lapse rate of $2^{\circ} \mathrm{C} / 1000{ }^{\prime}$ ) |  |
| DESTINATION FIELD: |  |
| Elevation: 5200'MSL | Altimeter setting: 30.12" |
| Temperature: $32^{\circ} \mathrm{C}$ | Wind: 350 ${ }^{\circ}$ @ 5kts. |
| Runway: 12 | Slope: 2\% Uphill |

EXAMPLE SUMMARY:

| SEGMENT | WEIGHT <br> (LBS.) | TIME <br> (MIN.) | DIST. <br> (NM) | FUEL <br> (L/LBS.) |
| :--- | :---: | :---: | :---: | :---: |
| Taxi | 7799 | 6 | - | $48 / 85$ |
| Takeoff | 7714 | 2 | - | $60 / 106$ |
| Climb | 7608 | 16.9 | 63 | $255 / 451$ |
| Cruise | 7157 | 40 | 183 | $283 / 501$ |
| Descent | 6656 | 9 | 29 | $50 / 88$ |
| Approach | 6568 | 5 | - | $40 / 71$ |
| Landing | 6497 | - | - | - |
| Totals |  | 78.9 | 275 | $736 / 1302$ |

(Flight time with no approach is 67.4 minutes)
QUICK, for a cross country flight at or above 15,000', no wind, use the following numbers for fuel flow and speed:

500 liters first 30 MINUTES.
500 liters per HOUR for the remainder.
250kt TAS average.
For the example, the time and fuel would be: 66 minutes. 800 liters.

## FUEL QUANTITY AND WEIGHT

Assuming the aircraft ZFW is 5500lbs. with two pilots enter the table at the current fuel load proceeding across to find aircraft weight.

The example plans a fuel load of 1300L. Entering the table at 1300 L and proceeding right to find the aircraft weight of 7799.4 lbs .

Additionally, this table may be used to convert liters into gallons or pounds.

## PERFORMANCE

## TAXI FUEL

Use 8 liters per minute for taxi fuel burn. The burn is less at idle however eight liters per minute is an average taking into consideration higher power settings needed for taxi and engine run-up. If an extended engine run-up is performed add 20 liters per minute for the time above $80 \%$ to the taxi fuel burn.

## STALL SPEEDS

Enter the table at the actual aircraft weight or interpolate between the weights closest to the actual weight.

The example plans a take off weight of 7714 lbs . Interpolate between 7497lbs and 7938lbs. to arrive at the stall speeds for 7714lbs. actual or next higher weight. For the example use the data for 7938lbs.

92/Clean
88/Takeoff
83/Landing

## WIND COMPONENT CHART

Enter the table at " 0 " proceeding outward on the angle difference between wind direction and the runway heading to the wind velocity arc. Proceed straight left to determine the headwind/tailwind component or proceed straight down to determine the crosswind component.

The example plans a takeoff from runway 30L with the wind $60^{\circ}$ to the right of runway heading at 10kts. Enter the table at 0 and proceed outward on the $60^{\circ}$ angle to the 10 kt . wind velocity arc. Proceed left to find a 5kt. headwind component or straight down to find an 8 kt . crosswind component.

## DENSITY ALTITUDE

Enter the table at the pressure altitude and proceed down to the density altitude adjacent to the current temperature. Linear interpolations may be necessary to determine exact density altitude.

The example plans a takeoff from an airport at 900'MSL with the altimeter setting of 29.82"HG. Knowing that $1 " \mathrm{HG}=1000$ ' of altitude it is determined that there is 100 ' difference between the MSL and pressure altitude. Being that the altimeter setting is less than the standard of 29.92" add the difference to the MSL altitude to find a pressure altitude of 1000'. If the altimeter setting had been higher than standard, the difference would be subtracted.

Enter the table at 1000' pressure altitude and proceed down adjacent to the current temperature of $27^{\circ} \mathrm{C}$ to find the density altitude of 2600'.

Additionally, this table may be used to convert temperatures between Fahrenheit and Celsius.

QUICK, enter the table at or the next higher pressure altitude and proceed down adjacent to the current or next higher temperature to find the density altitude.

## TAKEOFF

## Fuel:

For planning use 30 liters per minute for the time takeoff power is applied to when it is reduced to $97 \%$ for climb, normally 1000'AGL.

## Performance data:

1.) Enter the table at the actual weight and density altitude or interpolate as necessary between the weights and density altitudes closest to the actual conditions to find the takeoff data for the actual weight and density altitude.
2.) Make a correction, if needed, for headwind or tailwind as directed at the bottom of the respective table. (There is intentionally a slight difference between the corrections for the two takeoff tables.)
3.) Make a correction, if needed, for runway slope as indicated at the bottom of the table.

The example plans a takeoff from an elevation of $900^{\prime} \mathrm{MSL}(2,600$ ' D.A.) at a weight of 7714 lbs . with a five knot headwind and $1 \%$ downhill runway slope.

Step 1, Interpolate between the weights of 7497lbs. and 7938 lbs . at 2 K and 4 K to find the data for 7714 lbs . Then interpolate between the 2 K and 4 K interpolated data to find the data for 2.6 K .


## PERFORMANCE

Step 2, Subtract 10\% for the five knot headwind.

$$
\begin{gathered}
\frac{7714 / 2.6 \mathrm{~K}-10 \% / \mathrm{HW}}{2747 / 94} \\
4523 / 94 \\
3849 / 103
\end{gathered}
$$

Step 3, Subtract 2\% for the 1\% downhill slope from ground roll and distance to clear 50' obstacle. Do not make a correction to the accelerate stop distance.

| 7714/2.6K-10\%/HW-2\%/Slope |
| :---: |
| $2692 / 94$ |
| $4523 / 94$ |
| $3772 / 103$ |

The data displayed in each data block is as follows:
Ground Roll Distance/Liftoff Speed Accelerate Stop Distance/Abort Speed
Distance to Clear a 50 Obstacle/Speed at Obstacle
This information is not only provided for quick reference but is also provided to illustrate the additional distance that is required to stop, if an abort is initiated at takeoff speed, and to clear a 50 obstacle. Consider this information carefully in your go/no go decision.

QUICK, enter the table and use the data for the actual weight and density altitude or, if necessary, the next higher weight and or density altitude.
For the example use the takeoff data for 7938lbs. at 4000' D.A., 7938/4K 3537/96 5866/66 4837/105
Corrections for wind and slope only need to be applied if they decrease aircraft performance or if the additional performance is required.
Corrections that decrease performance shall be rounded up and added to the distances.
For this example no corrections were made as they increased aircraft performance.

## CLIMB

1.) Enter the table at the actual weight at start of climb and density altitude at the top of climb or interpolate as necessary between the weights and density altitudes closest to the actual conditions to find the climb data for the actual weight and density altitude.
2.) Subtract the altitude to climb from the density altitude at top of climb to find the start of climb density altitude.
3.) Enter the table at the actual weight and density altitude at the start of climb or interpolate as necessary between the weights and density altitudes closest to the actual conditions to find the climb data for the actual weight and density altitude.
4.) Subtract the data found in step 3 from the data found in step 1 to find the climb data.

The example plans a climb from 1900' to 16,500 'MSL a difference of 14,600' (time \& fuel used for a climb up to 1000 'AGL is included in the takeoff segment).

Step 1, the density altitude at the top of climb is 18,200'. Interpolate between the weights 7497 and 7938 at 15 K and 20 K to find the climb data for 7608 lbs . Then interpolate between 15 K and 20 K interpolated data to find the climb data for 7608lbs at 18,200'D.A..


## PERFORMANCE

Step 2, Subtract 14,600' (altitude to climb) from the top of climb of 18,200' density altitude to find the start of climb density altitude of 3,600'.

Step 3, Interpolate between the weights 7497 lbs . and 7938 lbs . at 5 K to find the climb data for 7608 lbs . Then interpolate between the interpolated data for 5 K and sea level to find the climb data for 7608lbs. at 3,600'.


Step 4, Subtract the data found in step 3 from the data found in step 1 to find the climb data for 7608 lbs . from 3,600 ' to 18,200 ' density altitude.
$7608 / 3.6 \mathrm{~K}-18.2 \mathrm{~K}(16,500 \mathrm{MSL})$ 16.9 min .
62.7 nm

255L Fuel.
QUICK, enter the table and use the data for the next higher weight closest to the density altitude at top of climb then subtract the data for the density altitude closest to the start of start climb.

For the example start with the data at 7938lbs. at 20,000' D.A. and subtract the data for 7938lbs. at $5,000^{\prime}$ D.A. ( 15,000 ' difference) to find the climb data of:
20.4min.
77.6 nm .

298L of fuel

## PERFORMANCE

## CRUISE

1.) Enter the table at the actual weight and density altitude planned for cruise or interpolate as necessary between the weights and density altitudes closest to the actual conditions to find the cruise data for the actual weight and density altitude in the desired profile.

The example plans to cruise at an altitude of 16,500' MSL (18,200' D.A.) at best speed.

Step 1, Interpolate between the weights of 7056lbs. and 7938 lbs . at 15 K and 20 K in the speed profile to find the data for the actual weight of 7157 lbs . Then interpolate between 15 K and 20 K interpolated data to find the cruise data at 7157 lbs , at $18,200^{\prime} \mathrm{D} . \mathrm{A}$.

| 7056/15K | 7938/15K 7056/20K | $7938 \mathrm{~K} / 20 \mathrm{~K}$ |
| :---: | :---: | :---: |
| 94 | $94 \quad 94$ | 94 |
| 470 | $470 \quad 400$ | 400 |
| 221/.44 | $217 / .43$ 204/.45 | 199/.44 |
| 276/.59 | 271/.58 276/.69 | 269/.67 |


| 57/15K 7157/20K |  |
| :---: | :---: |
| 94 | 94 |
| 470 | 400 |
| 221/.44 | 204/.45 |
| 276/.59 | 276/.69 |
| 7157/18.2K |  |
| 94\% |  |
| 425LPH |  |
| 210/.45 (CAS/MACH) |  |
| 276/.65 (TAS/nm per liter of fuel) |  |

Note: For preflight planning purposes it may be advantageous to determine the top of descent point, utilizing the descent table, prior to performing cruise calculations.

# QUICK, enter the table and use the data for the closest weight for the next lowest density altitude for the proposed cruise density altitude in the desired profile. 

For the example use the cruise data for 15 K at 7056 lbs. in the speed profile. 7056/15K 94\% N 1 470LPH 221/. 44 (CAS/MACH) 276/.59 (TAS/nm per liter of fuel)

## DESCENT

1.) Enter the table at the density altitude at the top of descent or interpolate between the closest density altitudes to find the data for a descent to sea level.
2.) Subtract the altitude to descend from the density altitude at top of descent to find the density altitude at bottom of descent.
3.) Enter the table at that density altitude at bottom of descent or interpolate between the closest density altitudes to find the data for a decent to sea level.
4.) Subtract the data found in step 3 from the data found in step 1 to find the descent data from top of descent to the bottom of descent.

The example plans a descent from 16,500MSL to $6,700 \mathrm{MSL}$ (pattern altitude) a difference of 9,800'.
Step 1, Interpolate between the data for 15 K and 20 K to find the descent data for 19.3 K (19,300' D.A. using the destination conditions and the std. lapse rate of $2^{\circ} \mathrm{C} / 1000^{\prime}$ ). $\quad 15 \mathrm{~K}$

17
20K

50 21 64
114 19.3K 133 20
62
130

## PERFORMANCE

Step 2, Subtract 9,800' (altitude to descend) from the top of descent density altitude of 19,300' to find 9,500' (density altitude at the bottom of descent).

Step 3, Interpolate between 5K and 10K to find the descent data for 9.5 K .

| $\frac{5 K}{7}$ |  | $\frac{10 \mathrm{~K}}{11}$ |
| :---: | :---: | :---: |
| 19 |  | 34 |
| 24 | $\frac{9.5 \mathrm{~K}}{11}$ | 86 |
|  | 33 |  |
|  | 80 |  |

Step 4, Subtract the data found in step 3 from the data in step 1 to find the descent data from $16,500 \mathrm{MSL}$ to 6,700'MSL.

$$
\frac{16,500 ' \mathrm{MSL}-6,70 \mathbf{'}^{\prime M S L}}{9 \mathrm{~min} .} \begin{gathered}
29 \mathrm{~nm} . \\
50 \mathrm{~L} . \text { of fuel }
\end{gathered}
$$

QUICK, enter the table and use the data for the amount of altitude closest to the amount to descend.
For the example a descent of 9,800 ' is planned so use the data for 10K.

10K<br>11min.<br>34 nm .<br>86L. of fuel

## APPROACH/HOLDING FUEL

Use 8 liters per minute fuel burn* for flight time for: Holding
IFR approach VFR traffic pattern
*Burn based on 135kts IAS, clean, and not configuring for landing until reaching a point where a normal descent to a landing can be made.

## PERFORMANCE

## LANDING

1.) Enter the table at the actual weight and density altitude or interpolate as necessary between the weights and density altitudes closest to the actual conditions to find the landing data for the actual weight and density altitude.
2.) Make a correction, if needed, for headwind or tailwind as directed at the bottom of the table.
3.) Make a correction, if needed, for runway slope as indicated at the bottom of the table.

The example plans a landing at an elevation of 5200 'MSL ( 8,000 ' D.A.) at a weight of 6497 lbs . with a four knot tailwind and 2\% uphill runway slope.

Step 1, Interpolate between the weights of 6174lbs. and 6615 lbs . at 8 K to find the data for 6497 lbs .


Step 2, Add 8\% for a four knot tailwind.

$$
\begin{gathered}
\frac{6497 / 8 \mathrm{~K}+8 \% / \mathrm{TW}}{97 / 82} \\
2636 \\
3204
\end{gathered}
$$

Step 3, Subtract 1\% for the $2 \%$ uphill slope from ground roll and distance to clear 50' obstacle.

## PERFORMANCE

6497/8K+8\%/TW-2\%/Slope
97/82 approach/touchdown speeds 2583 landing distance 3140 distance to clear a 50' obstacle

Please keep in mind the landing tables are based on maximum braking.

QUICK, enter the table and use the data for the actual weight and density altitude or, if necessary, the next higher weight and or density altitude.

Corrections that decrease performance shall be rounded up and added to the distances.

Corrections for wind and slope only need to be applied if they decrease aircraft performance or if the additional performance is required.

For the example use the landing data for 6615lbs. at 8000' D.A.,

6615/8K 98/83<br>2472<br>2995

For the tailwind round up from 8\% to $10 \%$ then round that figure up and add it to the distances (i.e. 250' and 300' respectively).

$$
\begin{gathered}
\frac{6615 / 8 K+10 \% / T W}{98 / 83} \\
2722 \\
3295
\end{gathered}
$$

For this example only the correction for the tailwind was applied. The uphill slope would increase performance or shorten the distances.

## PERFORMANCE

## FUEL QUANTITY AND WEIGHT

| LITERS $=$ GALLONS $=$ POUNDS ${ }^{*}+$ A/C WEIGHT** |  |  |  |
| :---: | :---: | :---: | :---: |
| 100 | 26.4 | 176.9 | 5676.9 |
| 200 | 52.8 | 353.8 | 5853.8 |
| 300 | 79.2 | 530.6 | 6030.6 |
| 400 | 105.6 | 707.5 | 6207.5 |
| 500 | 132.0 | 884.4 | 6384.4 |
| 600 | 158.4 | 1061.3 | 6561.3 |
| 700 | 184.8 | 1238.2 | 6738.2 |
| 800 | 211.2 | 1415.0 | 6915.0 |
| 900 | 237.6 | 1591.9 | 7091.9 |
| 1000 | 264.0 | 1768.8 | 7268.8 |
| 1100 | 290.4 | 1945.7 | 7445.7 |
| 1200 | 316.8 | 2122.6 | 7622.6 |
| 1300 | 343.2 | 2299.4 | 7799.4 |

*BASED ON FUEL DENSITY OF 6.7LBS. PER GALLON. ** BASED ON ZERO FUEL WEIGHT OF 5500LBS.

STALL SPEEDS
AT 1G

| 5733LBS. | 6174LBS. | 6615LBS. |
| :---: | :---: | :---: |
| 78 | 81 | 84 |
| 74 | 77 | 80 |
| 70 | 73 | 76 |
| 7056 LBS. | 7497 LBS. | 7938 LBS. |
| 87 | 90 | 92 |
| 83 | 85 | 88 |
| 78 | 81 | 83 |

CLEAN / FLAPS \& GEAR UP
TAKEOFF / FLAPS $15^{\circ}$ \& GEAR DOWN LANDING / FLAPS $30^{\circ}$ GEAR DOWN

LINEAR INTERPOLATIONS ARE PERMISSIBLE.

WIND COMPONENT CHART


## DENSITY ALTITUDE X 1000'

| TEMP. | PRESSURE ALTITUDE X 1000' |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| ${ }^{\circ} \mathrm{F} /{ }^{\circ} \mathrm{C}$ | 12 | 13 | 14 | 15 | 16 | 17 |
| $80 / 27$ | 15.9 | 17.1 | 18.3 | 19.5 | 20.7 | 21.9 |
| $60 / 16$ | 14.8 | 16.0 | 17.2 | 18.4 | 19.6 | 20.8 |
| $40 / 4$ | 13.5 | 14.7 | 15.9 | 17.1 | 18.3 | 19.6 |
| $20 /-7$ | 12.2 | 13.4 | 14.7 | 15.9 | 17.1 | 18.3 |
| $0 /-18$ | 10.9 | 12.1 | 13.4 | 14.6 | 15.8 | 17.1 |
| $-20 /-29$ | 9.5 | 10.7 | 12.0 | 13.2 | 14.5 | 15.7 |
| $-40 /-40$ | 8.0 | 9.3 | 10.5 | 11.8 | 13.1 | 14.3 |


| TEMP. | PRESSURE ALTITUDE X $1000 \prime$ |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  <br> ${ }^{\circ} \mathrm{F} /{ }^{\circ} \mathrm{C}$ | 18 | 19 | 20 | 21 | 22 | 23 |
| $60 / 16$ | 22.0 | 23.2 | 24.4 | 25.6 | 26.8 | 28.0 |
| $40 / 4$ | 20.8 | 22.0 | 23.2 | 24.4 | 25.6 | 26.8 |
| $20 /-7$ | 19.6 | 20.8 | 22.0 | 23.2 | 24.4 | 25.6 |
| $0 /-18$ | 18.3 | 19.5 | 20.8 | 22.0 | 23.2 | 24.4 |
| $-20 /-29$ | 17.0 | 18.2 | 19.5 | 20.7 | 22.0 | 23.2 |
| $-40 /-40$ | 15.6 | 16.9 | 18.1 | 19.4 | 20.6 | 21.9 |

Note: 1"HG equals 1,000' altitude. If pressure is higher than standard subtract from MSL altitude for pressure altitude, if lower than standard add.

LINEAR INTERPOLATIONS ARE PERMISSIBLE.

## TAKEOFF PERFORMANCE

 FLAPS $15^{\circ}$, $\mathrm{N}_{1}$ 100\% AT BRAKES RELEASE PAVED, LEVEL, DRY SURFACE RUNWAY| D. | 5733LBS. | 6174LBS. | 6615LBS. |
| :---: | :---: | :---: | :---: |
| S. <br> L. | REMOVED FOR SAMPLE | $\begin{aligned} & 1570 / 85 \\ & 3104 / 85 \\ & 2563 / 92 \end{aligned}$ | REMOVED FOR SAMPLE |
| 2 0 0 0 | $\begin{aligned} & \text { REMOVED } \\ & \text { FOR } \\ & \text { SAMPLE } \end{aligned}$ | $\begin{aligned} & 1733 / 85 \\ & 3392 / 85 \\ & 2779 / 92 \\ & \hline \end{aligned}$ | REMOVED FOR SAMPLE |
| 4 0 0 0 | REMOVED FOR SAMPLE | $\begin{aligned} & 1986 / 85 \\ & 3717 / 85 \\ & 3032 / 92 \end{aligned}$ | REMOVED FOR SAMPLE |
| $\begin{aligned} & \hline 6 \\ & 0 \\ & 0 \\ & 0 \end{aligned}$ | $\begin{aligned} & \text { REMOVED } \\ & \text { FOR } \\ & \text { SAMPLE } \end{aligned}$ | $\begin{aligned} & 2256 / 85 \\ & 4060 / 85 \\ & 3339 / 92 \end{aligned}$ | REMOVED FOR SAMPLE |
| 8 0 0 0 0 | REMOVED FOR SAMPLE | $\begin{aligned} & 2563 / 85 \\ & 4475 / 85 \\ & 3699 / 92 \end{aligned}$ | REMOVED FOR SAMPLE |

GROUND ROLL DISTANCE / LIFTOFF SPEED ACCELERATE STOP DISTANCE I ABORT SPEED DISTANCE TO CLEAR A 50' OBSTACLE I SPEED AT OBSTACLE (DISTANCE IN FEET / SPEED IN KNOTS)
LINEAR INTERPOLATIONS ARE PERMISSIBLE. CORRECTIONS TO BE MADE IN THE FOLLOWING ORDER:

1) SUBTRACT 3\% FOR EACH KNOT OF HEADWIND.
2) ADD 4\% FOR EACH KNOT OF TAILWIND.
3) SUBTRACT 2\%FOR EACH 1\% DOWNHILL SLOPE.
4) ADD 6\% FOR EACH 1\% UPHILL SLOPE.
(CORRECTIONS FOR SLOPE ON ACC. STOP DIST. NIA.)

# CLIMB PERFORMANCE 

 FROM SEA LEVEL

TIME IN MINUTES. DISTANCE IN NM. FUEL IN LITERS.

* $\mathrm{N}_{1}$ must be reduced to $94 \%$ after 30 minutes.

LINEAR INTERPOLATIONS ARE PERMISSIBLE.
DOES NOT INCLUDE TAXI \& TAKEOFF FUEL.

## CRUISE PERFORMANCE 10,000' DENSITY ALTITUDE

|  | 6174LBS. | 7056LBS. | 7938LBS. |
| :---: | :---: | :---: | :---: |
| R | REMOVED | 87 | REMOVED |
| A | FOR | 390 | FOR |
| N | SAMPLE | $180 / .33$ | SAMPLE |
| G |  | $209 / .53$ |  |
| E |  |  |  |


|  | REMOVED | 90 | REMOVED |
| :---: | :---: | :---: | :---: |
| M | FOR | 440 | FOR |
| I | SAMPLE | $206 / .37$ | SAMPLE |
| D |  | $238 / .54$ |  |


| S | REMOVED | 94 | REMOVED |
| :---: | :---: | :---: | :---: |
| P | FOR | 530 | FOR |
| E | SAMPLE | $233 / .42$ | SAMPLE |
| E |  | $269 / .51$ |  |
| D |  |  |  |

PERCENT N 1
FUEL FLOW IN LITERS PER HOUR CAS / PERCENT OF MACH
TAS I NAUTICAL MILES PER LITER OF FUEL
FOR FLIGHTS WITHOUT EXTERNAL FUEL TANKS OR PYLONS INSTALLED, INCREASE SPEED AND NAUTICAL MILES PER LITER OF FUEL BY 4\%.

LINEAR INTERPOLATIONS ARE PERMISSIBLE.
SHADED VALUES ARE FOR INFORMATION ONLY AND ARE NOT RECOMMENDED FOR LONG RANGE CRUISE.

# DESCENT PERFORMANCE 

 $\mathrm{N}_{1} 65 \%$ 162KTS IAS TO SEA LEVEL SPEED BRAKES RETRACTED| D. | ALL |
| :---: | :---: |
| A. | WEIGHTS |
|  | 24 |
| $25 K$ | 78 |
|  | 148 |



TIME IN MINUTES.
DISTANCE IN NM.
FUEL IN LITERS.

## LINEAR INTERPOLATIONS ARE PERMISSIBLE.

DOES NOT INCLUDE APPROACH FUEL.

# LANDING PERFORMANCE 

FLAPS $30^{\circ}$ IDLE THRUST SPEED BRAKES EXTENDED MAXIMUM BRAKING PAVED, LEVEL, DRY SURFACE RUNWAY

| D. A. | 5292LBS. | 5733LBS. | 6174LBS. |
| :---: | :---: | :---: | :---: |
| S. <br> L. | REMOVED FOR SAMPLE | $\begin{aligned} & 92 / 77 \\ & 1840 \\ & 2346 \end{aligned}$ | REMOVED FOR SAMPLE |
| $\begin{aligned} & \hline 2 \\ & 0 \\ & 0 \\ & 0 \end{aligned}$ | REMOVED FOR SAMPLE | $\begin{aligned} & 92 / 77 \\ & 1931 \\ & 2437 \end{aligned}$ | REMOVED FOR SAMPLE |
| 4 0 0 0 | REMOVED FOR SAMPLE | $\begin{aligned} & 92177 \\ & 2021 \\ & 2563 \end{aligned}$ | REMOVED FOR SAMPLE |
| $\begin{aligned} & \hline 6 \\ & 0 \\ & 0 \\ & 0 \\ & \hline \end{aligned}$ | $\begin{aligned} & \text { REMOVED } \\ & \text { FOR } \\ & \text { SAMPLE } \end{aligned}$ | $\begin{array}{r} 92 / 77 \\ 2130 \\ 2635 \\ \hline \end{array}$ | REMOVED FOR SAMPLE |
| 8 <br> 0 <br> 0 <br> 0 | $\begin{aligned} & \text { REMOVED } \\ & \text { FOR } \\ & \text { SAMPLE } \end{aligned}$ | $\begin{aligned} & 92 / 77 \\ & 2237 \\ & 2779 \end{aligned}$ | REMOVED FOR SAMPLE |

APPROACH SPEED / TOUCHDOWN SPEED LANDING DISTANCE
LANDING DISTANCE TO CLEAR A 50' OBSTACLE (DISTANCE IN FEET / SPEED IN KNOTS) LINEAR INTERPOLATIONS ARE PERMISSIBLE. CORRECTIONS TO BE MADE IN THE FOLLOWING ORDER:

1) SUBTRACT 1\% FOR EACH KNOT OF HEADWIND.
2) ADD $2 \%$ FOR EACH KNOT OF TAILWIND.
3) SUBTRACT 1\%FOR EACH 2\% UPHILL SLOPE.
4) ADD 1\% FOR EACH 1\% DOWNHILL SLOPE.


## PILOT-PERF/\$45.00 US

